

Effect of Changing Heart Rate on the Ocular Pulse and Dynamic Biomechanical Behavior of the Optic Nerve Head

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53 **ABSTRACT**

54 **Purpose:** To study the effect of changing heart rate on the ocular pulse and the
55 dynamic biomechanical behaviour of the optic nerve head (ONH) using a
56 comprehensive mathematical model.

57

58 **Methods:** In a finite element model of a healthy eye, a biphasic choroid consisted of
59 a solid phase with connective tissues and a fluid phase with blood, and the lamina
60 cribrosa (LC) was viscoelastic as characterized by a stress-relaxation test. We
61 applied arterial pressures at 18 ocular entry sites (posterior ciliary arteries) and
62 venous pressures at four exit sites (vortex veins). In the model, the heart rate was
63 varied from 60 bpm to 120 bpm (increment: 20 bpm). We assessed the ocular pulse
64 amplitude (OPA), pulse volume, ONH deformations and the dynamic modulus of the
65 LC at different heart rates.

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67 **Results:** With an increasing heart rate, the OPA decreased by 0.04 mmHg for every
68 10 bpm increase in heart rate. The ocular pulse volume decreased linearly by
69 0.13 μL for every 10 bpm increase in heart rate. The storage modulus and the loss
70 modulus of the LC increased by 0.014 MPa and 0.04 MPa, respectively, for every 10
71 bpm increase in heart rate.

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73 **Conclusions:** In our model, the OPA, pulse volume, and ONH deformations
74 decreased with an increasing heart rate, while the LC became stiffer. The effects of
75 blood pressure / heart rate changes on ONH stiffening may be of interest for
76 glaucoma pathology.

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89 INTRODUCTION

90 Glaucoma is a complex, multifactorial disease. Although the pathogenic mechanism
91 of glaucoma has still not been well understood, it has generally been accepted that
92 various interlinked biomechanical and vascular pathways to glaucomatous injury are
93 involved, and that these are closely related to the optic nerve head (ONH)
94 biomechanics.¹⁻⁸ The ONH, and in particular the lamina cribrosa (LC), is a primary
95 site of interest during the development of glaucoma since it is the region where
96 retinal ganglion cell (RGC) axon damage occurs. Because the ONH is constantly
97 exposed to several loads in vivo (e.g. IOP, cerebrospinal fluid pressure (CSFP),
98 orbital fat pressure, optic nerve traction),^{6, 9-13} there is a general consensus that
99 knowing how 'robust' a ONH is could be a critical information for estimating the risk
100 of developing glaucoma.

101 To date, to assess the biomechanics of the ONH in vivo, the typical approach
102 has been to artificially manipulate IOP (e.g. with ophthalmodynamometry) while
103 observing the resulting deformations with optical coherence tomography (OCT).¹⁴⁻¹⁷
104 While such methods may have value from a research point of view, they may not be
105 easily translated clinically due to discomfort during the examination of the patients.
106 However, IOP is not constant but rather pulsatile, fluctuating constantly with the
107 cardiac cycle. The fluctuation of IOP with the heart rate has been known as the
108 ocular pulse and the difference between the systolic and diastolic IOP has been
109 termed the ocular pulse amplitude (OPA). In a previous study, we proposed a
110 framework to assess ONH biomechanics in vivo without artificially manipulating IOP.
111 ONH deformations can indeed be measured by using the ocular pulse as the load,¹⁸
112 and from such data, modelling can help us interpret these deformation data to derive
113 stiffness estimates for the ONH.¹⁹

114 This is however a complex engineering problem: the ONH tissues are
115 viscoelastic,^{7, 20, 21} which basically means that ONH stiffness is affected by the rate
116 of loading, or in other words, the duration of the cardiac cycle. Indeed, collagenous
117 soft tissues typically appear stiffer when they are loaded faster. This is a protective
118 mechanism for soft tissues to handle highly dynamic events.^{7, 20} Furthermore, it has
119 been shown clinically, that an increase in heart rate or a change in blood pressure
120 can also affect the OPA;^{22, 23} this will in turn affect the deformations of the ONH.

121 To measure the stiffness of the ONH using the ocular pulse as a natural load,
122 we believe it is critical to first build an understanding of how the heart rate and blood
123 pressure change the IOP (i.e. the OPA), and how they also affect the stiffness and
124 deformations of the ONH tissues. From a clinical point of view, if ONH tissues
125 appear stiffer, a physician should be able to tell whether this is because of a different
126 heart rate / blood pressure, or because of tissue remodelling from glaucoma. In this
127 study, we aim to build such an understanding using finite element (FE) modelling. In
128 the future, our proposed models could be combined with experimental data to
129 assess ONH stiffness in vivo.

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131

132 **METHODS**

133 Using FE modelling, we previously modelled the origin of the ocular pulse and its
134 effect on the ONH.¹⁹ We found that a change in arterial pressure (as that occurring
135 from diastole to systole) resulted in choroidal swelling, which in turn induced a
136 change in IOP (the OPA) due to the incompressibility of the vitreous. Both the OPA
137 and choroidal swelling were responsible for deforming the ONH tissues, and a
138 relatively large shearing of neural tissues was observed within the neuroretinal rim.
139 The vast majority of the trends we reported matched clinical and experimental data.

140 In this study, we used the same model, but we further defined the LC as a
141 viscoelastic material. Such viscoelastic properties were obtained experimentally
142 using uniaxial stress relaxation tests. Using our FE model, we then varied the heart
143 rate from 60 bpm to 120 bpm and studied its effect on: 1) the OPA, 2) the choroidal
144 pulse volume, 3) ONH deformations, and 4) LC stiffness.

145

146 **Three-Dimensional Geometry of the Ocular and Orbital Tissues**

147 The geometry of the three-dimensional eye model was adapted from our previous
148 studies.^{12, 19, 24} In summary, the eye globe and optic nerve were reconstructed from
149 magnetic resonance imaging images of a healthy subject. The corneoscleral shell
150 was assumed to be spherical with an outer diameter of 24 mm and thickness of 1
151 mm. The optic nerve was composed of three tissues: the nerve tissue, the pia mater
152 and the dura mater. A generic ONH geometry was constructed and embedded within
153 the corneoscleral shell, including the scleral flange, Bruch's membrane, the LC, the
154 prelaminar tissue and the border tissue of Elschnig and Jacoby as extensions of the

155 pia mater. The model was then meshed using 67,584 eight-node hexahedrons and
156 3,024 six-node pentahedrons (Figure 1). The mesh density was numerically
157 validated through a convergence test. The whole eye was reconstructed, and
158 symmetry conditions were not applied.

159

160 **Biomechanical Properties of the Ocular Tissues**

161 The sclera was modelled as a fiber-reinforced composite, as described in our
162 previous paper.²⁵ The neural tissues and Bruch's membrane were modelled as
163 isotropic elastic materials.²⁶ The pia and dura were modelled as Yeoh materials, as
164 characterized from experiments with porcine eyes.²⁴ As performed in our previous
165 study, we modelled the choroid as a biphasic material comprising a solid phase and
166 a fluid phase (i.e. blood) to allow for changes in blood pressure during the cardiac
167 cycle and the movement of blood within the choroid.¹⁹ All biomechanical parameters
168 are listed in **Table 1**.

169

170 **Viscoelastic Properties of the Lamina Cribrosa**

171 In order to characterize the response of the LC under dynamic loading such as the
172 heart rate, we studied its viscoelastic properties. Since the viscoelasticity properties
173 of the LC have not been reported in the literature yet, we conducted uniaxial stress
174 relaxation tests of the LC of seven porcine eyes.

175 Experiments were performed in accordance to the ARVO (Association for
176 Research in Vision and Ophthalmology) statement for the Use of Animals in
177 Ophthalmic and Vision Research. The experimental procedure followed the
178 previously described methodology designed for the sclera.^{27, 28} In brief, seven fresh
179 porcine eyes were collected and cleaned of all extraorbital tissues. After dissecting
180 the eye and cutting the optic nerve, the retina and choroidal layers were removed. A
181 customized device was used to cut a scleral strip (orientation: inferior to superior)
182 with the LC in its center (width: 1.2 mm; Figure 2). Mineral oil was applied to the
183 specimen surface to maintain hydration. Each sample was mounted between the two
184 grips of the uniaxial tensile tester (Instron 5848; Instron. Inc., Norwood, MA, USA)
185 with the LC exposed in the center (Figure 2c). The sample was subjected to 10
186 cycles of preconditioning at 1% strain prior to the stress relaxation test. The sample
187 was then subjected to a maximum of 5% strain at a rate of 1% per second, followed
188 by a relaxation period of 300s at constant stress. These strain levels were chosen as

189 they are typically exhibited in vivo under physiological conditions (during eye
190 movements or change in IOP).¹⁰ The thickness measurements of the LC (mean:
191 0.628mm) were obtained by spectral-domain optical coherence tomography
192 (Spectralis OCT, Heidelberg Engineering, Heidelberg, Germany) and were used to
193 compute the tensile stress. The averaged stress values of seven porcine eyes were
194 fitted with a linear viscoelastic model incorporating a reduced relaxation function to
195 characterize the viscoelastic properties of the LC.²⁸ A typical stress relaxation curve
196 is shown in Figure 2d.

197

198 **Boundary and Loading conditions**

199 Two sets of boundary conditions were applied to ensure numerical stability. First, the
200 orbital apex of the optic nerve was fixed to model its connection to the optic canal.
201 Second, the eye globe was fixed near the equator on two opposite sides with four
202 nodes on each side. This was carried out to improve stability and to avoid such
203 boundary conditions from having an impact on the ONH deformations.

204 We applied a baseline IOP of 15 mmHg to the inner limiting membrane and a
205 baseline CSFP of 11.3 mmHg to the arachnoid space (Figure 3).²⁹ As described
206 previously, we applied prescribed fluid pressures on the choroidal layer to mimic the
207 blood flow inlets (long and short posterior ciliary arteries [PCAs]) and outlets (vortex
208 veins).¹⁹ The arterial pressure was varied between 70.8 and 93 mmHg to mimic the
209 diastolic and systolic changes of the ophthalmic artery pressure.³⁰ A constant blood
210 pressure of 15 mmHg was applied at the four vortex veins exits out of the choroid.³¹
211 In our model, it was the pressure difference between the PCAs and vortex veins that
212 drove the choroidal blood flow, allowing the choroid to swell during the cardiac cycle.

213

214 **Changing the Heart Rate from 60 to 120 bpm**

215 We aimed to understand the impact of different heart rates on the ocular pulse, ONH
216 deformations, and LC stiffness. Hence, four models were implemented with the heart
217 rate ranging from 60 to 120 bpm with an increment of 20 bpm. All the boundary
218 conditions and material properties were kept constant, such that only the heart rate
219 varied.

220

221 **FE Processing to Predict the OPA, Pulse Volume, and ONH Deformations**

222 All FE models were solved with FEBIO v2.8.5 (Musculoskeletal Research
223 laboratories, University of Utah, Salt Lake City, UT, USA).³² The OPA was estimated
224 by first assuming that the vitreous was incompressible as performed in our previous
225 study.¹⁹ This is a reasonable assumption because the vitreous mostly consists of
226 water, which is also incompressible, and is gas-free. Therefore, the volume of the
227 vitreous body was constrained to remain constant during choroidal swelling in all our
228 simulations. Since our model aimed to reproduce choroidal swelling during the
229 cardiac cycle, such a swelling will try to deform and change the volume of the
230 vitreous body. Since the vitreous body was constrained as incompressible, an
231 internal pressure needed to be applied to maintain its volume. This pressure term is
232 an output of our model and can be understood as the OPA.

233 More specifically, each model was implemented in three steps as shown in
234 Figure 4. The initial step applied boundary conditions and loads including baseline
235 IOP, CSFP and ophthalmic arterial pressure and vortex vein pressure. During the
236 second step, a 5000s relaxation period was applied due to the viscoelasticity of the
237 LC. All the boundary conditions and loads remained unchanged. During the final step,
238 we imposed a volume constraint to the inner limiting membrane to ensure the
239 incompressibility of the vitreous.¹⁹ The CSFP, baseline IOP and vortex vein pressure
240 were kept constant; the ophthalmic arterial pressure varied from diastole to systole
241 periodically following a sinusoidal profile for two cycles.

242 The post processing was performed using MATLAB (v2018; Mathworks,
243 Natick, MA, USA). For each model, we reported the OPA, the pulse volume, the
244 diastole-to-systole displacements of the LC and of the pre-lamina tissue. In addition,
245 we characterized the stiffness of the LC at different heart rates in the central region
246 along the radial, circumferential and longitudinal directions (Figure 5).

247

248 **Characterizing LC Stiffness with Changing Heart Rate**

249 The stiffness of the LC can be characterized by computing its dynamic modulus, as
250 typically performed for dynamic mechanical analyses.²⁰ Since the ocular pulse
251 induced a cyclic deformation of the LC, the LC strain ‘input’ can be represented as:

$$252 \quad \varepsilon = \varepsilon_0 \sin(\omega t + \delta_\varepsilon) \quad (1)$$

253 where ε_0 , δ_ε , and ω are the peak strain amplitude, strain phase shift and angular
254 frequency of the harmonic excitation, respectively. Since the LC only exhibits small
255 strains, the LC can be approximated to be linear viscoelastic.³³ Hence, the resulting

256 sinusoidal stress ‘output’ would differ in phase from the ‘input’ strain depending on
257 the viscoelastic properties of the LC, and can be expressed as:

$$258 \quad \sigma = \sigma_0 \sin(\omega t + \delta_\sigma) \quad (2)$$

259 where σ_0 and δ_σ are the peak stress amplitude and stress phase shift, respectively.

260 The phase delay between the stress and the strain due to viscoelastic effects is
261 known as the phase lag δ , i.e. the difference between δ_ε and δ_σ (Figure 6). The
262 dynamic mechanical properties of the LC can now be represented by the complex
263 dynamic modulus, consisting of the storage modulus (elastic component) and the
264 loss modulus (viscous component). It is defined as:

$$265 \quad E^* = \frac{\sigma}{\varepsilon} = E' + iE'' \quad (3)$$

266 where E' is the storage modulus, E'' is the loss modulus, and i the unit imaginary
267 number. The storage and loss moduli are related to the phase lag through the
268 following equations:

$$269 \quad E' = E * \cos(\delta), \quad (4a)$$

$$270 \quad E'' = E * \sin(\delta) \quad (4b)$$

271

272 For each heart rate, we computed the storage and loss moduli in the central
273 region of the LC (composed of one element). We first computed the Lagrange strain
274 and Cauchy stress tensors, and estimated the diastole-to-systole Lagrange strain
275 and Cauchy stress profiles along three directions (radial, circumferential, and
276 longitudinal). Each strain/stress profile was then fitted with equations (1-2) to
277 determine the peak strain/stress amplitudes and the phase shifts. From these data
278 we extracted the phase lag, and thus the storage and loss moduli of the LC central
279 region along 3 directions: radial, circumferential, and longitudinal.

280

281 **RESULTS**

282

283 **Effect of the Heart Rate on the Ocular Pulse**

284 For each model, the pulsating arterial pressure during the cardiac cycle
285 resulted in choroidal swelling (increase in pulse volume), which in turn increased the
286 IOP (the delta change in IOP being the OPA). The IOP and the pulse volume as
287 functions of time are shown in Figure 7 for two cycles at a heart rate of 60 bpm.

288 We also found that both the OPA and the pulse volume decreased with an
289 increasing heart rate (Figure 7). On average, the OPA and the pulse volume
290 decreased by 0.04 mmHg (2.7%) and 0.13 μ L (2.8%), respectively for every 10 bpm
291 heart rate increment.

292

293

294 **Effect of the Heart Rate on ONH Deformations**

295 During the cardiac cycle, the ONH moved posteriorly (diastole-to-systole) and
296 anteriorly (systole-to-diastole). The diastole-to-systole displacement of the central
297 anterior LC point was 5.8 μ m at a heart rate of 60 bpm and decreased by 0.1 μ m for
298 every 10 bpm heart rate increment (Figure 8a-c).

299 We also observed that the prelamina (neural tissue anterior to the lamina) and
300 the parapapillary retina moved along opposite directions during the cardiac cycle.
301 Specifically, from diastole to systole, the prelamina moved posteriorly (as highlighted
302 in red in Figure 8d), whereas the parapapillary retina (highlighted in black in Figure
303 8d) moved anteriorly. This resulted in a net shearing of the neural tissues in the
304 neuro-retinal rim. This shearing amount (difference between the prelamina
305 displacement and the parapapillary retina displacement) also decreased with an
306 increasing heart rate. On average, the shearing amount reduced by 0.12 μ m for
307 every 10 bpm heart rate increment (Figure 8f).

308

309 **Effect of the Heart Rate on LC stiffness**

310 The storage and loss moduli were computed in the central region of the LC for
311 3 orientations (radial, circumferential, and longitudinal). They all followed the exact
312 same trend and all increased with an increasing heart rate. On average, the storage
313 modulus increased by 0.014 MPa, and the loss modulus by 0.04 MPa, for every 10
314 bpm heart rate increment. This indicates that the lamina cribrosa will appear stiffer
315 with a higher heart rate.

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323 **DISCUSSION**

324 In this study, we used FE modelling to study the impact of the heart rate on the
325 ocular pulse and its biomechanical impact on the ONH. Our model predicted that the
326 OPA, pulse volume and ONH deformations decreased with an increasing heart rate.
327 In addition, the LC became stiffer at faster heart rates. These findings may help
328 develop technologies to finely assess the biomechanical properties of the ONH in
329 vivo.

330

331 **The OPA and the Pulse Volume Decreased with an Increasing Heart Rate**

332 With an increase in heart rate, both the OPA and the pulse volume reduced when
333 simultaneously the ophthalmic arterial and venous vein pressures were kept
334 constant. A faster heart rate is associated with a shorter duration for each cardiac
335 cycle, suggesting that the volume of blood being pushed into the choroid would be
336 reduced for each pulse. Our results are also consistent with a previous clinical
337 study,²³ in which all the subjects were fitted with cardiac pacemakers and the heart
338 rate was altered by resetting the pacemakers. Neither IOP nor systolic-diastolic
339 blood pressures were found to be significantly altered during the experiments,
340 suggesting that the heart rate was one of the main contributing factor causing a
341 reduction in OPA.

342 It has also been observed that a short period of dynamic exercise can also
343 lead to a reduction in OPA and ocular pulse volume.³⁴⁻³⁶ However, the impact of
344 exercise is complex as it involves changes in multiple physical parameters including
345 not only the IOP and heart rate, but also the systolic and diastolic blood pressures,
346 and blood distribution in the body. Although heart rate and blood pressures involve
347 separate mechanisms, exercises would induce an increase in both heart rate and
348 blood pressures.³⁷ The systolic and diastolic blood pressures are related to the
349 ocular pulse through the ocular perfusion pressure (OPP), defined as the difference
350 between the mean blood pressure and IOP. In one study, there was a significant
351 reduction in IOP, and an increase in OPP immediately after strenuous exercise
352 (resting: heart rate= 68 ± 7.9 bpm, IOP= 19.8 ± 5.4 mmHg, OPP = 51.2 ± 4.9 mmHg;
353 after exercise: heart rate= 125 ± 24.9 bpm, IOP= 14.3 ± 5.0 mmHg, OPP= 56.9 ± 7.5

354 mmHg).³⁶ Our models could potentially be used to reproduce more complex
355 scenarios such as those.

356

357 **ONH deformations and Neural Tissue Shear Decreased with an Increasing**

358 **Heart Rate**

359 Our model predicted that ONH deformations decreased with an increasing heart rate.
360 It has been shown that isometric exercise caused a significant increase in the mean
361 arterial blood pressure and pulse rate, and decreased the fundus pulsation amplitude,
362 as measured by laser interferometry.²² Despite changes in the mean arterial blood
363 pressure, reduced fundus pulsation amplitude may indicate a decrease in ONH
364 deformations at a faster heart rate, which is consistent with our predicted results.

365 From diastole to systole, the shearing amount refers to the anterior movement
366 of the parapapillary retina due to the choroidal expansion and the posterior ONH
367 deformation due to both choroidal swelling and the OPA. With an increase in heart
368 rate, it is expected that the shearing amount would decrease due to the reduced
369 OPA and pulse volume. This shearing phenomenon has been observed in-vivo in
370 humans using low-coherence tissue interferometry.¹⁸

371

372 **The LC Became Stiffer with an Increasing Heart Rate**

373 Our model predicted that the dynamic modulus of LC increased with an increasing
374 heart rate. Similar phenomena have also been observed in other viscoelastic
375 biological tissues such as the cornea^{38, 39} intervertebral discs,⁴⁰ and other
376 biomaterials.⁴¹ The dynamic modulus characterizes the stiffness of a material in
377 response to dynamic loading, and it can differ from its static behaviour since
378 viscoelastic materials typically become more rigid with a faster loading rate.^{38, 39} The
379 static modulus describes the elasticity of a tissue at 'equilibrium', whereas the
380 dynamic modulus provides information about the instant stiffness of a material. For
381 instance, for the cornea, the dynamic properties are likely dominated by the
382 rearrangement of the extracellular matrix (mainly through diffusion of water) upon
383 changes in stress, whereas the static properties are more closely related to the
384 collagen structure.⁴² Histological studies have shown that the morphology of the LC,
385 as a porous, reticulated and multi-lamellar sieve-like structure, mainly comprises of
386 laminar beams consisting of elastin fibres and collagen fibrils (type I and III).⁴³ Hence,
387 it is likely that the dynamic and static responses of the LC are also dominated by

388 different components, and both may change differently during the progression and
389 development of glaucoma.

390

391 **Clinical Relevance to Glaucoma Pathogenesis**

392 At first view, a faster heart rate may be beneficial for the eye. First, it resulted in a
393 smaller OPA and hence smaller ONH deformations. A larger deformation would yield
394 larger strain/stress fluctuations within the LC, which may have an impact on the
395 retinal ganglion cell axons and the vascular capillaries. This is also consistent with
396 the fact that a larger OPA has been observed in chronic angle-closure glaucoma and
397 suspected open-angle glaucoma subjects.⁴⁴

398 Second, a faster heart rate also resulted in lower neural tissue shear, which
399 may limit axonal damage in the neuroretinal rim region.⁴⁵⁻⁴⁷ As discussed in our
400 previous work, repeated shearing of axons in the neuroretinal rim region could
401 potentially contribute to axonal damage. The neuroretinal rim is indeed a region that
402 exhibits a mechanical discontinuity: it is where RGC axons follow a sharp turn to
403 enter the disc. In this region, a reduction in Bruch's-membrane-opening minimum-
404 rim-width (BMO-MRW) has been observed clinically in glaucoma and in elderly
405 individuals.⁴⁵⁻⁵⁰ Hence, decreasing shearing with a faster heart rate may be seen as
406 'mechanically protective'.

407 Third, the LC was found to stiffen with an increasing heart rate, which could
408 provide better support to the RGCs and vasculatures. Pseudoexfoliation (PEX)
409 syndrome is a systemic disorder of the elastic fiber system which can lead to PEX
410 glaucoma. It has been reported that the stiffness of the LC in PEX eyes is 40% less
411 than that in normal eyes as evaluated by atomic force microscopy.⁵¹ This decrease
412 in LC stiffness may increase susceptibility to IOP-induced glaucomatous optic nerve
413 damage as observed in PEX eyes, and thus, dynamic stiffening of the LC may also
414 be seen as beneficial.

415 However, the situation may be more complex as the effects of dynamic
416 loading at the cellular level has remained elusive yet. The response of cells to
417 deformation is dependent on both the magnitude and the rate of mechanical strain.
418 Some studies have shown that short-term strain or stress variations can lead to
419 cellular injury in neurons and neuron-like cells.⁵²⁻⁵⁴ Future research is required to
420 better understand the link between dynamic loading and RGC axonal injury at the
421 micro or cellular scale.

422

423 **Understanding The Clinical Implications of LC Stiffening**

424 During the development and progression of glaucoma, the connective tissues of the
425 ONH undergo constant remodelling (including stiffening in the moderate/severe
426 stages) and extensive structural changes.⁵⁵ The extracellular matrix remodelling are
427 usually characterized by fibrotic changes associated with cellular and molecular
428 events such as myofibroblast activation that could drive further tissue fibrosis and
429 stiffening.⁵⁶ However, as discussed herein, the LC also gets stiffer with an increased
430 heart rate. Ex vivo strain measurement shows that the stiffness of the LC increases
431 with age.⁵⁷ It is believed that the change in LC stiffness due to the change in heart
432 rate and aging involves different mechanisms. Our results only reflect the short-term
433 impact of a raised heart rate and we do not know whether the stiffening of the lamina
434 will become chronic or whether other homeostatic mechanisms might reverse these
435 changes in the longer term. If an increase in dynamic LC stiffness is proved to be
436 beneficial, it is possible to modulate heart rate in the longer term via pharmacological
437 means. Finally, it is important to note that, while assessing the material properties of
438 the LC from the ocular pulse, physicians should be able to distinguish whether a
439 change in LC stiffness is because of a different heart rate/blood pressure, or
440 because of tissue remodelling. This information may be helpful to predict glaucoma
441 progression.

442 **Limitations**

443 Our study has several limitations. First, our model did not consider the regional
444 variations in the scleral thickness and stiffness, which are known to exist in monkeys,
445 canines, and humans.^{20, 58, 59} The regional variations may affect the prediction of the
446 OPA.

447 Second, the choroid was simplified and modelled as a biphasic material,
448 consisting of a porous solid phase (connective tissues) and a fluid phase (blood). In
449 addition, the permeability of the choroid was approximated grossly from the vascular
450 resistance, the average diameter of the choroid and the blood viscosity.¹⁹ The
451 complex microvasculature architecture, as well as the blood flow of the choroid,
452 cannot be fully captured by this description. For instance, the segmental distribution
453 of PCAs⁶⁰ and the autoregulatory capacity of the choroid^{22, 61} were not taken into
454 account in our model. Furthermore, the PCAs and vortex veins were not modelled
455 explicitly but represented by prescribed fluid pressures. Future work may need to

456 assess the permeability of the choroid experimentally and also consider more
457 complex material models to better describe the behaviour of the pulsatile choroidal
458 blood flow.

459 Third, our model did not account for the blood circulation within the LC and
460 other pulsatile components including those from the retina, central retinal artery and
461 the CSFP. These pulsations may affect the LC deformations as well. The pulsation
462 of the CSFP is phase-shifted with respect to the ocular pulse, such that the CSFP
463 peak occurs slightly before that of the IOP.^{62, 63} The phase difference between the
464 IOP and CSFP may lead to dynamic fluctuations of the translaminal pressure
465 gradient, resulting in different ONH deformation profiles. The contribution of these
466 pulsatile components may be important and should be considered in future studies.

467 Fourth, the geometry of the eye was constructed from a single eye model and
468 the dimensions of the ONH were taken as average measurements from the literature.
469 However, the ocular and ONH geometries can vary widely across individuals and
470 thus may influence the predicted ocular pulse significantly. In our model, the retina,
471 choroid and BM were simplified as a uniform layer throughout the eye. We aim to
472 take regional variations in tissue thickness into consideration in future work.

473 Fifth, we experimentally measured the viscoelastic material properties of the
474 porcine LC in this study. It is possible that the LC exhibits different viscoelastic
475 properties across species. In addition, the LC was simplified as an isotropic and
476 homogeneous material; the complicated laminar microarchitecture was not taken into
477 account. Micro-level modelling of the laminar beams predicted higher strain and
478 stress than those predicted by macro-scale models of the ONH.⁶⁴ The mean strain of
479 the laminar beams varies greatly across different nonhuman primates and depends
480 on the 3D geometry of each eye's ONH connective tissues.^{64, 65} Models
481 incorporating the micro-level laminar beams may be considered in the future.

482 Sixth, for simplicity and as a first approach, we only modelled the
483 viscoelasticity of the LC and not that of other tissues such as the choroid and the
484 sclera. We focused on the LC only as it is a tissue that has been observed under
485 dynamic loading¹⁸ and because it plays a critical role in glaucoma as the main site of
486 damage. More complex models will be needed in the future to better understand how
487 scleral and choroidal viscoelasticity could interact with the LC.

488 Seventh, the results shown only reflect the short-term impact of a raised heart
489 rate and we do not know whether the stiffening of the lamina will become chronic or

490 whether other homeostatic mechanisms might reverse these changes in the longer
491 term.

492 Eighth, the LC was modelled as a uniform structure. We did not take into
493 account potential differences in the anatomy and biomechanical properties of the
494 various layers of the LC, nor did we consider lateral movements of the LC in
495 dependence of changes of the examined parameters and in dependence of the
496 obliqueness of the optic nerve canal and the spatial relationship between Bruch's
497 membrane opening and the lamina cribrosa position.^{66, 67}

498 **Conclusions**

499 In this study, we used FE modelling to study the ocular pulse and the impact of the
500 heart rate on ONH deformations. We found that the OPA, the pulse volume the ONH
501 deformation reduce at a faster heart rate. Our models also indicated that the LC
502 becomes stiffer with increasing heart rate. These results will help us develop
503 technology to assess the biomechanics of the ONH in vivo by using the ocular pulse
504 as a natural load.

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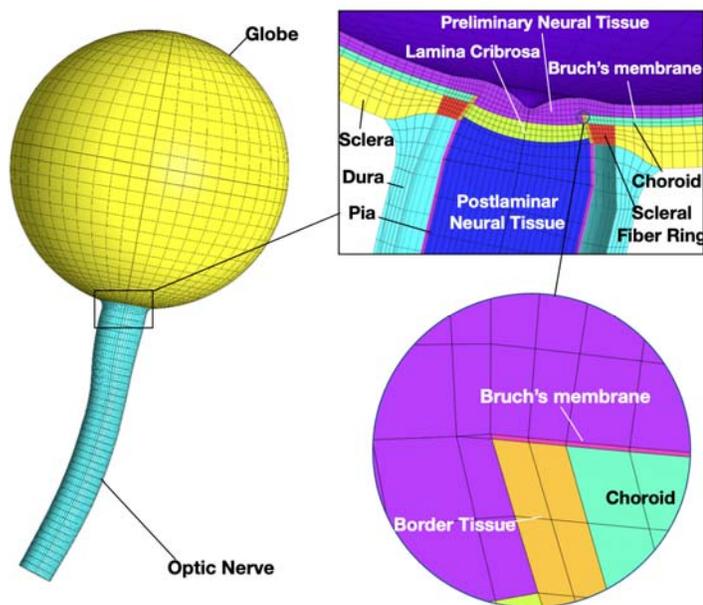
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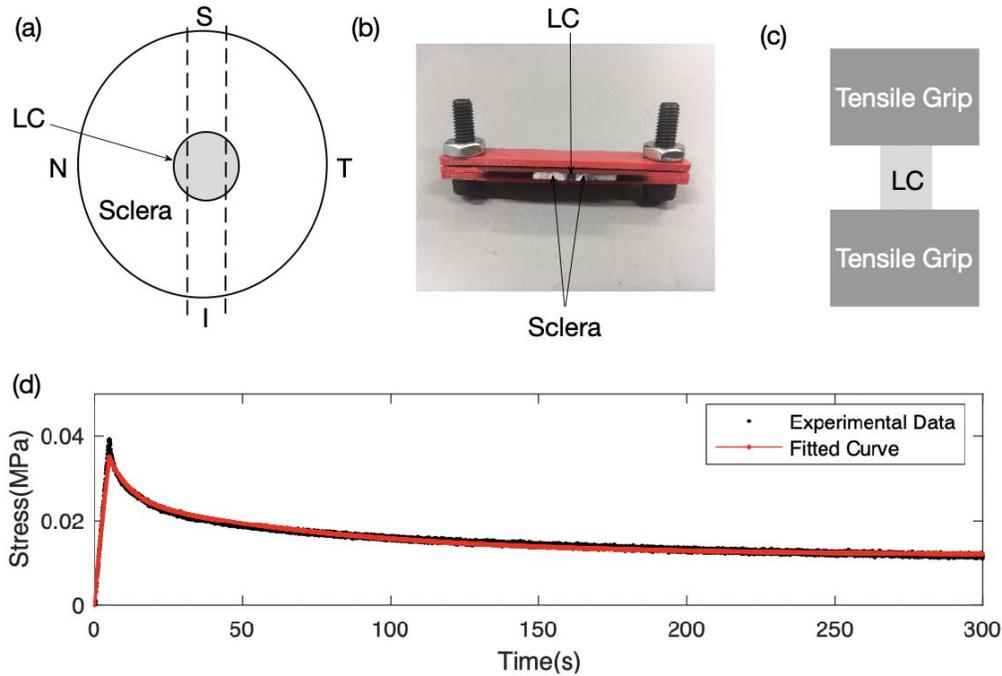
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Figures and Tables



546
547 **Figure 1.** Reconstructed geometry and FE mesh of the whole eye model adopted
548 from Jin.¹⁹ ONH structures (including the LC, sclera, neural tissues, choroid, BM,
549 border tissue, pia and dura) were reconstructed using average measurements from
550 the literature.^{9, 19, 24, 26, 68}

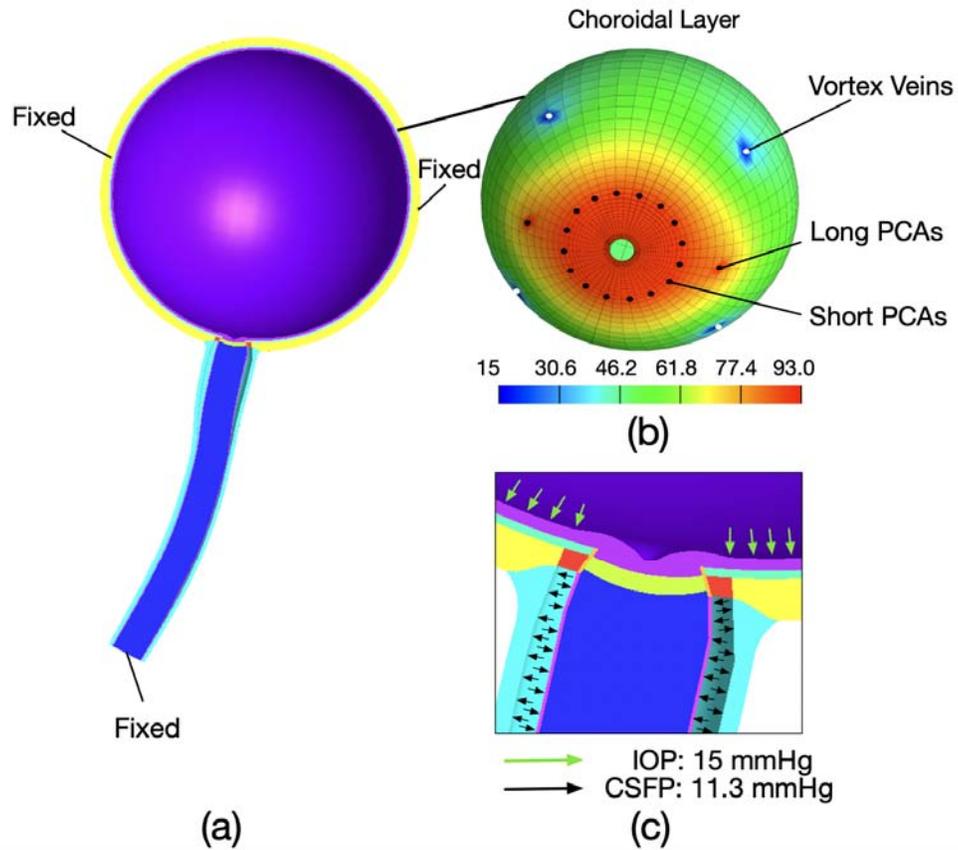
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Figure 2. (a) Schematic showing the scleral strip with the LC in its center. The uniaxial tensile specimen was obtained by using a customized device (shown in b) to obtain a fixed width of 1.2 mm. It was then clamped between the tensile grips (shown in c) with the LC exposed in its centre. (d) A typical stress relaxation experimental test dataset for an LC sample fitted with a linear viscoelastic model curve.²⁸

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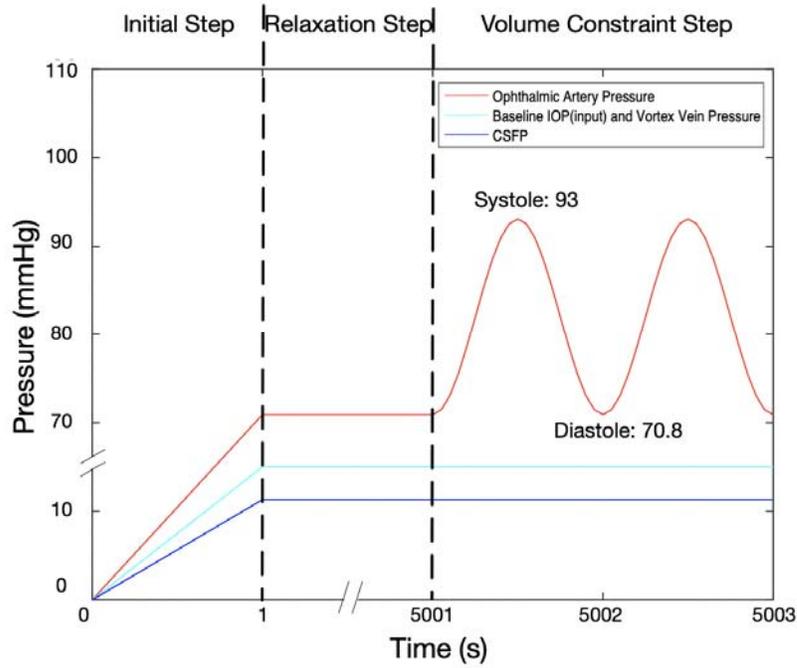


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568 **Figure 3:** (a) Half eye geometry and boundary conditions: fixed optic nerve at the
569 orbital apex and fixed sclera nodes near the equator on two opposite sides. (b)
570 Choroidal with the nodes where arterial blood pressure (short and long PCAs) and
571 venous blood pressures (vortex veins) were applied. (c) ONH region illustrating the
572 pressure loads (IOP, CSFP) applied in each model.

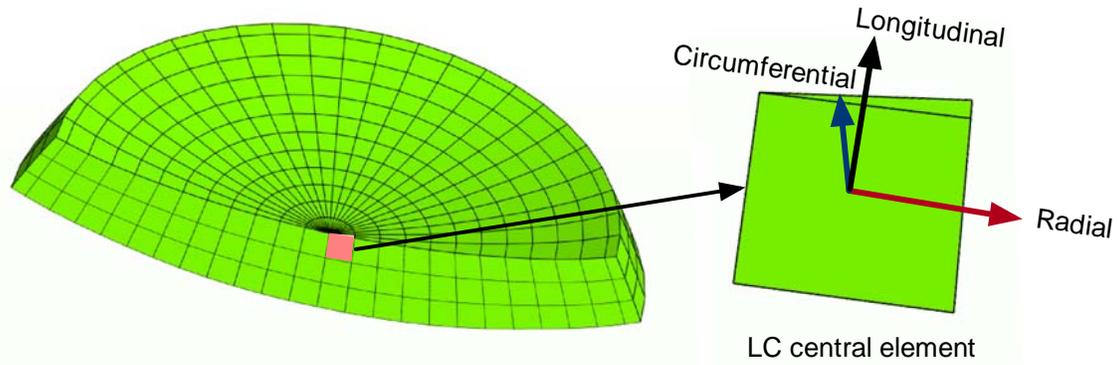
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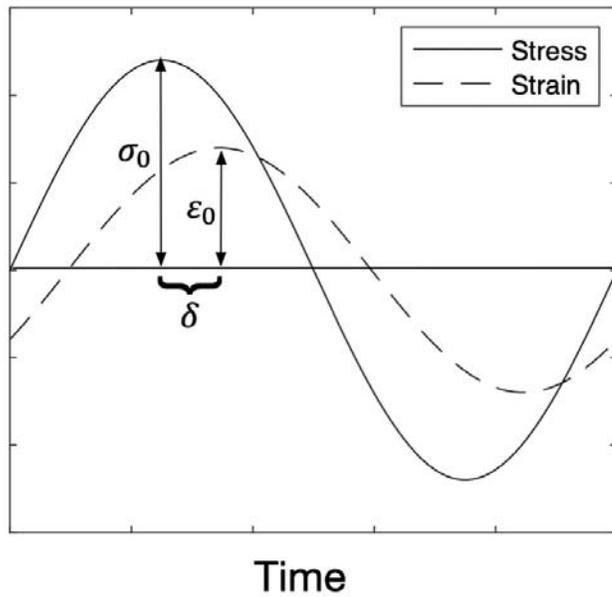
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Figure 4. Profiles of different pressure loads.



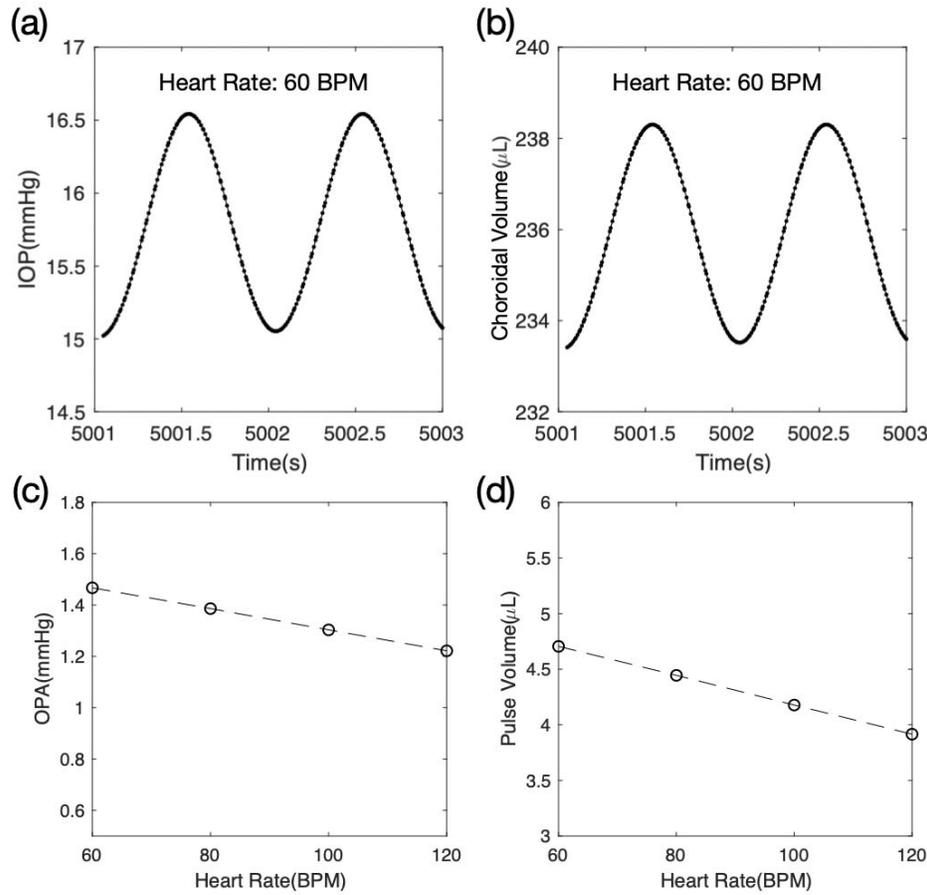
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Figure 5: Cross-section of the LC illustrating the local coordinates (radial, circumferential and longitudinal) for one central element.



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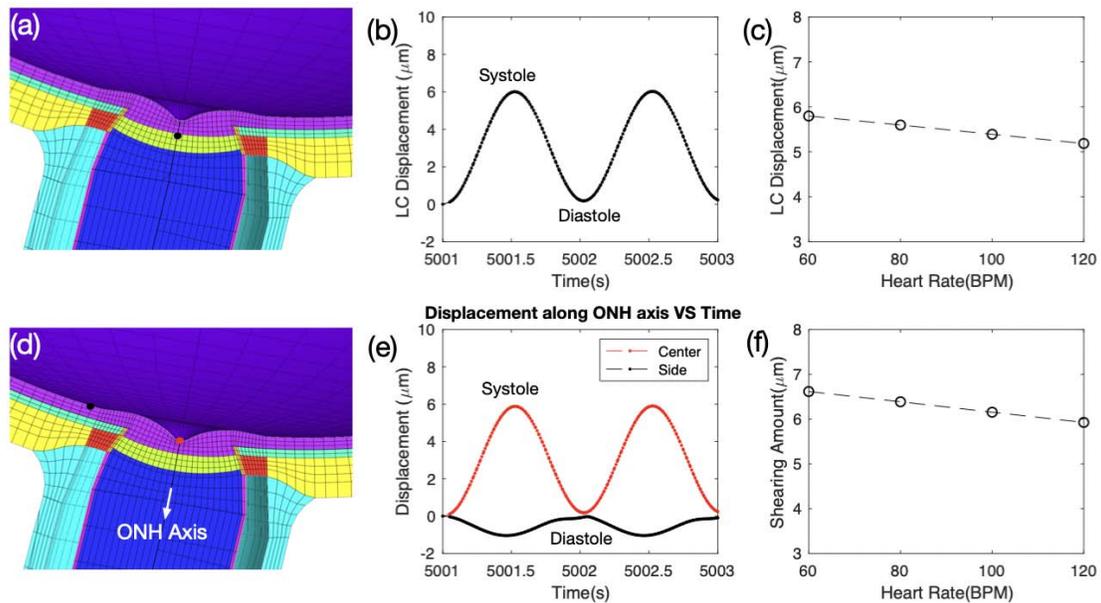
Figure 6. Schematic representation of the strain and stress profiles as a function of time in calculating the dynamic properties of the LC.



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Figure 7. (a,b) IOP and choroidal volume over two cycles at a heart rate of 60 BPM. (c,d) Change of the OPA and the pulse volume (PV) with heart rate.

LC displacement and shearing amount



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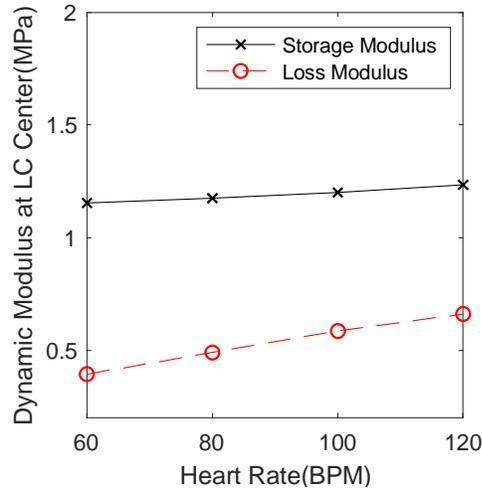
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Figure 9. Change of the storage and loss moduli of the LC center with the heart rate.

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660 **TABLES**

661 **Table 1.** Tissue biomechanical properties used for all models

Tissue	Constitutive Model	Biomechanical Properties	References
Sclera	Mooney-Rivlin Von Mises distributed fibers	c1 = 0.285 MPa c3 = 0.0137 MPa c4 = 658.125 kf = 2 (scleral ring) kf = 0 (other region of sclera) θ_p : preferred fiber orientation	Girard et al. ²⁵
LC	Viscoelastic	Instantaneous modulus = 8.49 MPa Equilibrium modulus = 0.49 MPa Long-term time constant = 272 s Short-term time constant = 8.33 s	Porcine tissue experiment (this study)
Neural tissue	Isotropic elastic	Elastic modulus = 0.03 MPa Poisson's ratio = 0.49	Miller ⁶⁹
BM	Isotropic elastic	Elastic modulus = 10.79 MPa Poisson's ratio = 0.49	Chan et al. ⁷⁰
Choroid	Biphasic	solid volume fraction: 0.55 Solid matrix: Neo-Hookean Elastic modulus = 0.06 MPa Poisson's ratio = 0 Permeability: 45037 mm ² /MPa.s	Jin et al. ¹⁹
Dura	Yeoh model	C1 = 0.1707 MPa C2 = 4.2109 MPa C3 = -4.9742 MPa	Wang et al. ²⁴
Pia	Yeoh model	C1 = 0.1707 MPa C2 = 4.2109 MPa C3 = -4.9742 MPa	Wang et al. ²⁴

Border Tissue	Isotropic elastic	Elastic modulus = 10.79MPa Poisson's ratio = 0.49	Chan et al. ⁷⁰
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